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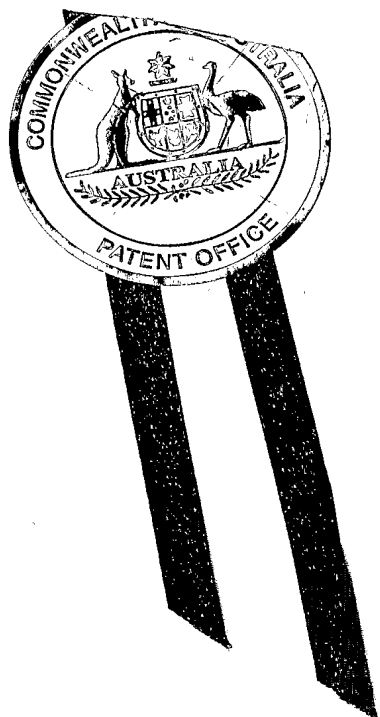


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I, JANENE PEISKER, TEAM LEADER EXAMINATION SUPPORT AND SALES hereby certify that annexed is a true copy of the Provisional specification in connection with Application No. 2004901688 for a patent by TECHNOLOGICAL RESOURCES PTY LIMITED as filed on 29 March 2004.



WITNESS my hand this  
Thirty-first day of March 2005

A handwritten signature in dark ink, appearing to read 'J. R. + C.'.

JANENE PEISKER  
TEAM LEADER EXAMINATION  
SUPPORT AND SALES

AUSTRALIA  
Patents Act 1990

**PROVISIONAL SPECIFICATION**

**Applicant(s):**

TECHNOLOGICAL RESOURCES PTY LIMITED  
A.C.N. 002 183 557

**Invention Title:**

DIRECT SMELTING PLANT

The invention is described in the following statement:

DIRECT SMELTING PLANT

5 The present invention relates to direct smelting plant for producing molten metal in pure or alloy form from a metalliferous feed material such as ores, partly reduced ores and metal-containing waste streams.

10 A known direct smelting process, which relies principally on a molten metal layer as a reaction medium, and is generally referred to as the HIs melt process, is described in International Patent Publication WO 96/31627 (International Patent Application PCT/AU96/00197) in the name of the applicant. The HIs melt process as described in the International application comprises:

- 15 (a) forming a bath of molten iron and slag in a vessel;
- (b) injecting into the bath:
- (i) a metalliferous feed material, typically metal oxides; and
- 20 (ii) a solid carbonaceous material, typically coal, which acts as a reductant of the metal oxides and a source of energy; and
- (c) smelting metalliferous feed material to metal in the metal layer.

25

The term "smelting" is herein understood to mean thermal processing wherein chemical reactions that reduce metal oxides take place to produce liquid metal.

30 The HIs melt process also comprises post-combusting reaction gases, such as CO and H<sub>2</sub> released from the bath in the space above the bath with oxygen-containing gas and transferring the heat generated by the post-combustion to the bath to contribute to the thermal energy required to smelt the metalliferous feed materials.

35

The HIs melt process also comprises forming a transition zone above the nominal quiescent surface of the bath in which there is a favourable mass of ascending and thereafter descending droplets or splashes or streams of

molten metal and/or slag which provide an effective medium to transfer to the bath the thermal energy generated by post-combusting reaction gases above the bath.

5 In the Hismelt process the metalliferous feed material and solid carbonaceous material is injected into the metal layer through a number of lances/tuyeres which are inclined to the vertical so as to extend downwardly and inwardly through the side wall of the smelting vessel and into the lower region of the vessel so as to deliver  
10 the solids material into the metal layer in the bottom of the vessel. To promote the post combustion of reaction gases in the upper part of the vessel, a blast of hot air, which may be oxygen enriched, is injected into the upper region of the vessel through the downwardly extending hot  
15 air injection lance. Offgases resulting from the post-combustion of reaction gases in the vessel are taken away from the upper part of the vessel through an offgas duct.

The Hismelt process enables large quantities of  
20 molten metal to be produced by direct smelting in a single compact vessel. However, in order to achieve this it is necessary to transport hot gases to and from the vessel, to transport the metalliferous feed material to the vessel and to transport the molten metal product and slag away  
25 from the vessel all within a relatively confined area. This requires the installation of various major ancillary components in the plant. For example, there will generally be gas heating stoves and ducting for supply of heated input gas to the vessel; solids feed equipment for  
30 feeding ore and coal to the vessel which equipment may include apparatus for pre-heating the ore; offgas ducting and offgas treatment apparatus such as offgas scrubbing and demisting apparatus and molten metal and slag tapping and handling equipment. All of these components must  
35 operate continuously through a smelting operation which can be extended over a long period and it is necessary to provide for access to the vessel and ancillary components for maintenance and lifting of equipment between smelting operations.

Building a direct smelting plant of the kind described above presents major problems in that it is necessary to erect various kinds of major equipment sourced from different manufacturers at a single site area. The present invention facilitates offsite prefabrication and installation of one of the major plant components namely the iron making unit comprising the direct smelting vessel. This unit may also comprise a vessel access tower which may envelope the vessel.

10 The invention provides a method of constructing and thereafter installing at a direct smelting plant site a smelting unit comprising a direct smelting vessel, which method comprises the steps of prefabricating away from a predetermined location of the plant site a plurality of  
15 vessel modules to be brought together to form the vessel, each module comprising a circumferential vessel wall section, transporting the prefabricated vessel modules to the predetermined location and depositing them sequentially on top of one another and joining them  
20 together by one or more circumferential connections between successive circumferential wall sections of the modules to form a unitary direct smelting vessel.

The circumferential vessel wall sections of the modules may be formed of steel plate and the or each  
25 connection between successive circumferential wall sections may be a circumferential weld joining those wall sections. The weld may be a continuous horizontal weld made on site after the modules to be connected have been deposited on top of one another.

30 The vessel modules may comprise a base module and one or more further modules to be deposited above the base module.

The further modules may include an intermediate module and an upper module, the intermediate module being  
35 deposited onto the base module and connected to an upper part of the base module and the upper module being deposited on and connected to an upper part of the intermediate module.

The base module may include a hearth and a forehearth for discharging molten metal. The hearth and forehearth may be lined with refractory bricks after installation at the smelting plant site.

5           The intermediate vessel module may comprise a generally cylindrical barrel section provided with a tap hole for discharging molten slag.

The upper vessel module may be provided with an outlet for off gases.

10           At least one of the further modules may be prefabricated so as to be internally lined with water cooling panels connected to water inlet and outlet connections on the exterior of the circumferential wall section of that module.

15           The intermediate module and the upper module may both be prefabricated with water cooling panels connected to water inlet and outlet connectors on the exterior of the circumferential wall sections of those modules.

20           The base module may also be partially lined with water cooled panels.

The method may also comprise the steps of prefabricating away from said predetermined location a plurality of tower modules to be brought together to form a vessel access tower, transporting the prefabricated tower modules to the predetermined location and depositing them sequentially on top of another and joining them together to form the tower.

25           The tower modules may be formed such that the tower will extend about the vessel at the completion of installation of the vessel and the tower.

30           At least one pair of the tower modules may be connected together at the same level as the connection between a pair of the vessel modules.

35           At least some of the tower modules may be installed before the vessel modules about which they are to extend are installed, the latter vessel modules being deposited downwardly into the interior of the installed tower modules.

The tower structure may carry water supply and return piping and the construction and installation method may include the further step of connecting that supply and return piping to the water inlet and outlet connectors of the water cooling panels.

In order that the invention may be more fully explained, one particular embodiment will be described in some detail with reference to the accompanying drawings in which

Figure 1 is a diagrammatic perspective view of a direct reduction vessel;

Figure 2 is an elevation of the direct reduction vessel;

Figure 3 is a plan of the vessel;

Figure 4 is an elevation of a base module of the vessel;

Figure 5 is a sectional elevation of the base module;

Figure 6 is an elevation of an intermediate vessel module;

Figure 7 is an elevation of an upper vessel module;

Figure 8 illustrates the arrangement of cooling panels lining a main cylindrical barrel part of the vessel;

Figure 9 is a development of the cooling panels shown in Figure 8;

Figure 10 is a development showing cooling panels fitted to the vessel;

Figure 11 is an elevation of one of the cooling panels fitted to the cylindrical barrel section of the vessel;

Figure 12 is a plan of the panel shown in Figure 11;

Figure 13 is a cross-section on the line 13-13 in Figure 11;

Figure 14 is a front view of the cooling panel illustrated in Figure 11;



Figure 15 illustrates a detail of the cooling panel;

Figures 16 and 17 illustrate details of the connection of a cooling panel to the vessel shell;

5 Figure 18 illustrates lower centre and upper modules of a vessel access tower; and

Figure 19 is an elevation of an assembled tower enveloping a smelting vessel.

10 The drawings show a direct smelting vessel 11 suitable for operation by the HIs melt process as described in International Patent Publication WO 96/31627. Vessel 11 has a hearth 12 that is lined with refractory bricks; side walls 14 which form a generally cylindrical barrel extending upwardly from the hearth; an upper barrel  
15 section 15 and a roof 16 leading to an offgas chamber 20 with an outlet 17 for offgases; a forehearth 18 for discharging molten metal continuously; and a tap hole for discharging molten slag.

Vessel 11 is designed to be fitted with a  
20 downwardly extending gas injection lance 21 for delivering a hot air blast into the upper region of the vessel and eight solids injection lances (not shown) extending downwardly and inwardly through the side walls for injecting iron ore, solid carbonaceous material and fluxes  
25 entrained in an oxygen deficient carrier gas into the bottom part of the vessel.

Gas injection lance 21 receives an oxygen enriched hot air flow through a hot gas delivery duct that extends from a hot gas supply station located on the plant  
30 site in the vicinity of the reduction vessel 11.

The offgas outlet 17 is connected to an offgas duct 24 which transports the offgas away from the reduction vessel 11 to a treatment station located on the plant site a short distance away from the reduction  
35 vessel 11.

Hot metal is continuously tapped from vessel 11 through forehearth 18 and flows through appropriate launders to ladles by which it is transported to a desulphurization and casting station.

Slag continuously tapped from vessel 11 flows through slag launders to slag pits located behind vessel.

Vessel 11 is prefabricated off site in three modules 11A, 11B and 11C which are then transported to the direct melting plant site and hoisted by a crane and deposited sequentially on top of one another and joined together by welding to form a unitary vessel. Module 11A is a base module fabricated as a steel plate shell comprising a cylindrical lower barrel 31 for the vessel closed by a bottom floor 32. An outer steel plate shell 33 for the forehearth 18 projects radially outwardly from the lower part of barrel 31. Barrel 31 has a cylindrical circumferential wall 34 fitted with lifting trunions 35 at circumferential spacing to enable the whole module 11A to be lifted by a crane and deposited on site. The lower part of barrel 31 and the forehearth shell 33 are subsequently lined with refractory bricks to form the vessel hearth and forehearth. The lower part of barrel 31 is provided with an access door 36 to allow access for bricking and subsequent maintenance within the vessel.

The intermediate vessel module 11B is comprised of a cylindrical steel plate section forming an upper barrel 37 of the vessel. This barrel has a cylindrical circumferential wall 38 on which there are mounted eight circumferentially spaced upwardly and outwardly inclined tubular sockets 39 to mount the solids injection lance.

The cylindrical wall of barrel 31 of base module 11A is of the same diameter as the cylindrical wall of barrel 37 of module 11B. The upper rim of the cylindrical wall of the base module and the lower rim of the cylindrical wall of module 11B are chamfered so that when the two modules are fitted together a V shaped groove is formed to enable the two modules to be connected by a continuous horizontal full penetration weld around the two wall sections to be joined.

The upper part of the circumferential wall 37 of vessel module 11B is formed as an upwardly and inwardly inclined roof section 40 having an upper rim 42 of lesser diameter than the lower part of that peripheral wall.

Upper vessel module 11C comprises a cylindrical circumferential wall 44 of the same diameter as the upper rim of the circumferential wall of module 11B and the respective abutting rims of these two modules are  
5 chamfered to form a V shaped groove when the two come together to receive a continuous circumferential weld run horizontally around the walls to be connected. Module 11B forms the offgas chamber 20 for the upper part of the vessel and includes the offgas outlet 17 in the form of a  
10 flanged tubular spigot for connection to the offgas duct 24. The upper end of the offgas chamber 20 is closed by a circular lid 43 provided with an opening to receive the hot air injection lance for the vessel.

The circumferential walls of the intermediate  
15 vessel module 11B and the upper vessel module 11C are lined internally with water cooling panels 51, 52, 53, 54, 55.

The cooling panels consist of a set of forty-eight panels 51 lining an upper part of the  
20 cylindrical barrel section of base module 11A and the cylindrical barrel section 37 of the module 11B, a set of sixteen panels 52 lining the tapering roof section 40 of module 11B, and four panels 53, twenty panels 54 and eleven panels 55 lining those parts of the module 11C  
25 forming the offgas chamber 50.

The construction of panels 51 and the manner in which they are mounted on the cylindrical barrel 37 of module 11B is illustrated in Figures 11 to 17. As shown in Figures 8 to 10, these panels are disposed in 6  
30 vertically spaced tiers of arcuate panels spaced circumferentially of the vessel, there being eight individual panels 31 in each tier. A typical panel 51 is comprised of a coolant flow tube 56 bent to form inner and outer panel sections 57, 58 of zigzag formation. Coolant  
35 inlet and outlet tubular connectors 62 extend from the inner panel section at suitable locations and typically at one end of each panel. Panels 51 are of elongate arcuate formation with a curvature to match the curvature of the

cylindrical barrel section 37 of the module 11B and the module 11A.

5 A set of four mounting pins 63 are connected to the zigzag tubular formation of the outer panel section 58 by means of connector straps 64 so as to project laterally outwardly from the panel. Each connector strap 64 is fastened at its ends to adjacent tube segments of the inner panel section and extends between its ends outwardly across a tube segment of the outer panel section in the 10 manner shown most clearly in Figure 15. The connector straps 64 are generally V-shaped with the root of the V-shape curved to fit snugly about the tube segment of the outer panel section. The pins 63 are welded to the connector straps so as to extend outwardly from the roots 15 of the V-shapes. The connecting straps serve to brace the panels by holding the tube segments securely in spaced apart relationship at multiple locations distributed throughout the panels, resulting in a strong but flexible panel construction.

20 The mounting pins 63 are extended through openings 65 in the vessel wall and tubular protrusions 66 surrounding the openings 65 and protruding outwardly from the shell. The ends of pins 66 project beyond the outer ends of the tubular protrusions 66 and are connected to 25 the outer ends of those protrusions by welding annular metal discs 67 to the pins and protrusions thus forming connections exteriorly of the shell in a way which seals the openings 65.

In similar fashion the inlet and outlet 30 connectors, 62 for the panel project outwardly through openings 68 in the vessel wall and through and beyond tubular protrusions 69 surrounding those openings and protruding outwardly from the vessel and connections are made by welding annular discs 71, between the connectors 35 62 and the protrusions 69. In this way, each panel 51 is mounted on the vessel wall through the four pins 63 and the coolant connectors 62 at individual connections

exteriorly of the shell. The pins and coolant connectors are a clearance fit within the tubular protrusions tubes 66, 69 and the panel is free to move to accommodate thermal expansion and contraction movements or movements  
5 caused by pressure or contact with material within the vessel.

The pins 63 and the coolant inlet and outlet connectors 62 for each panel respectively are oriented so as to project laterally outwardly from the panel in  
10 parallel relationship to one another and so as to be parallel with a central plane extended laterally through the panel radially of the vessel so that the panel can be inserted and removed by bodily movement of the panel inwardly or outwardly of the cylindrical barrel of the  
15 vessel.

The gaps 53 between the circumferentially spaced panel 51 must be sufficient to enable the trailing outer edges of a panel being removed to clear the inner edges of the adjacent panels when the panel to be removed is  
20 withdrawn inwardly of the vessel 11 along the direction of the pins 66 and connectors 63. The size of the gaps required is dependant on the length of the arcuate panels and therefore the number of panels extending the circumference of the barrel section 37. In the  
25 illustrated embodiment there are eight circumferentially spaced panels in each of the six tiers of panels 51. It has been found that this allows minimal gaps between the panels and ensures proper cooling of refractory material at the gaps. Generally for satisfactory cooling it is  
30 necessary to divide each tier into at least six circumferentially spaced panels.

Refractory retainer pins 70 are butt welded to the coolant tubes of panels 51 so as to project inwardly from the panels and act as anchors for the refractory  
35 material sprayed out the panels. Pins 70 may be arranged in groups of these pins radiating outwardly from the

respective tube and arranged at regular spacing along the tube throughout the panel.

The panels 53 and 54, being fitted to cylindrically curved sections of the vessel, are formed and mounted in the same fashion as the panels 51 as described above, but some of the panels 54 are shaped in the manner shown in Figure 10 so as to fit around the offgas outlet 17.

The panels 52 and 55, being fitted to tapered sections of the vessel, are generally conically curved in the manner shown in the illustrated development of Figure 10. Except for this variance in shape. However, these panels are also formed and mounted to the shell in similar fashion to the panels 51, each being fitted with mounting pins projecting laterally outwardly from the panel and a pair of inlet/outlet coolant connectors at opposite ends of the panels, the pins and connectors being extended through openings in the shell and connected to tubes projecting laterally outwardly from the shell to form connections exteriorly of the shell which seal the openings and provide a secure mounting for the panels while permitting some freedom of movement of the panels.

Figures 18 and 19 show a vessel access tower 73 formed in three modules 73A, 73B and 73C. This tower is constructed so that in the final installation it can extend about and substantially envelop the vessel 11. Tower module 73A is a base module comprising a steel framework 74 with a central opening 75 to receive the base module 11A of the vessel. Module 73B is a centre tower module comprising a framework 76 of generally U shaped formation to fit around the intermediate and upper modules 11B and 11C of the vessel. Upper tower module 73C is designed to fit down onto an upper part of tower module 73B to extend over the top of the upper part of the vessel and provide access to the hot air blast duct and the hot air blast lance 21.

Tower modules 73A and 73B are designed to come together and to be connected by welding at the same level

as the connection between the base module 11A and the intermediate module 11B of the vessel. These two tower modules carry water supply and return piping comprising U shaped supply and return manifolds 81 and vertical supply and return pipes 82 for individual connection to the water panel inlet and outlet connectors 62, these connections being made by flexible hose connections to the supply and return pipes.

The vessel modules 11A, 11B and 11C and the tower modules 73A, 73B and 73C can be fabricated off site and brought to the plant for installation as part of the iron making unit for the plant. Normally the vessel would be prefabricated in a factory specializing in heavy metal fabrications and with appropriate heavy duty lifting and welding equipment.

After fabrication the individual vessel and tower modules are transported to the direct smelting plant site for installation. The order in which the various tower and vessel modules are lifted sequentially into place can be varied. Typically the tower base module 73A would be installed as a first step. The base module of the vessel could then be lifted and dropped into position within the base module of the tower. Alternatively the central tower section 73B could be lifted into position and connected to the tower module 73A before installing the successive vessel modules 11A, 11B and 11C. The upper tower module 73C is installed as a final step in the assembly.

The illustrated equipment has been advanced by way of example only. The physical construction of this equipment could be varied considerably as could the precise order in which the various modules are brought together. It is to be understood that such variations can be made without departing from the scope of the invention to be protected.





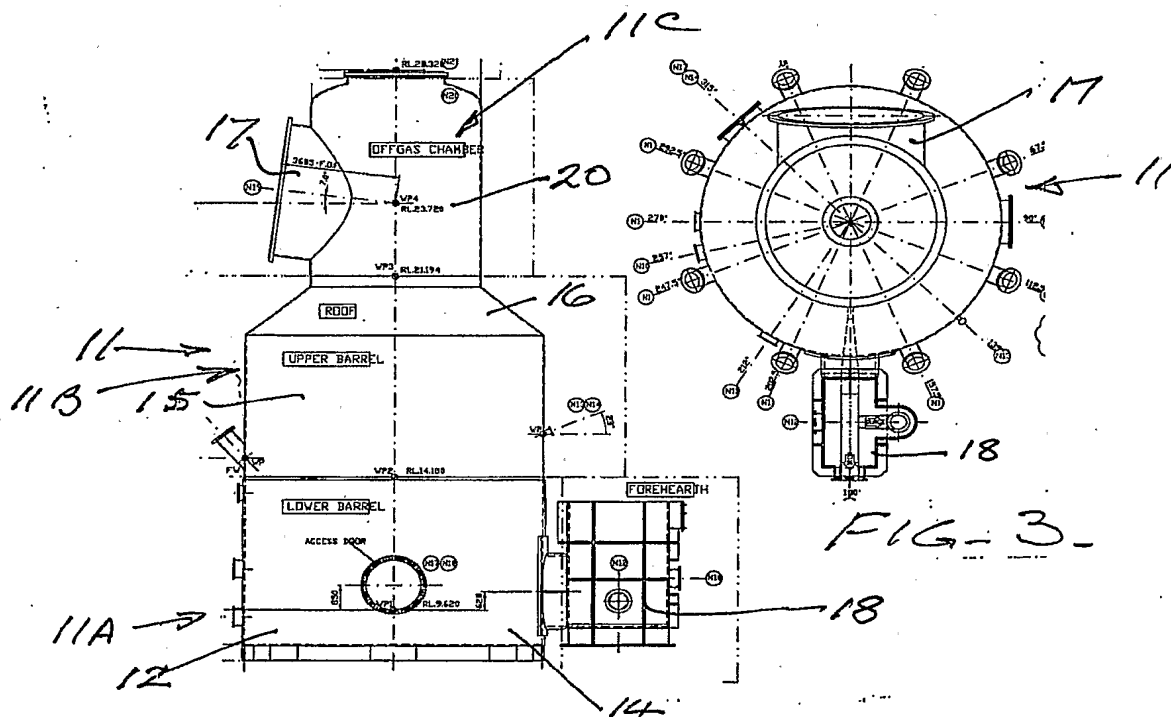


FIG. 2

FIG. 3

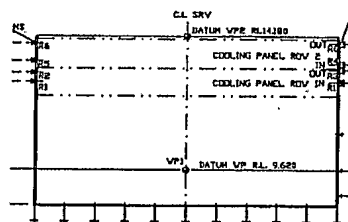


FIG-5

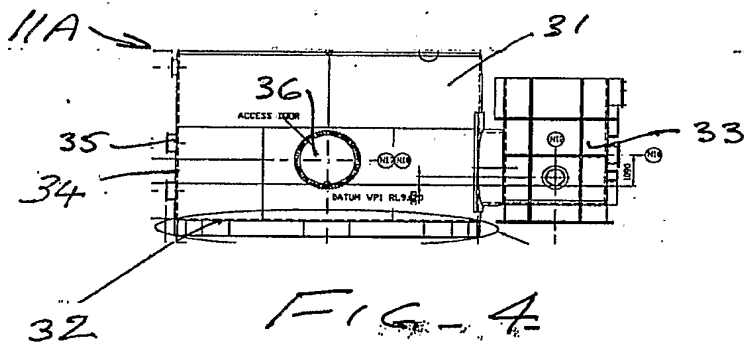


FIG-4

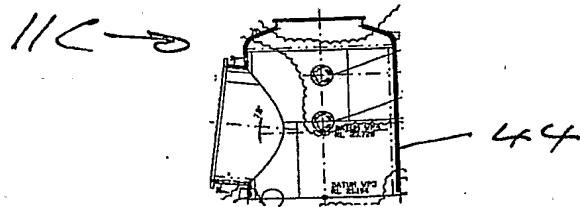


FIG. 7

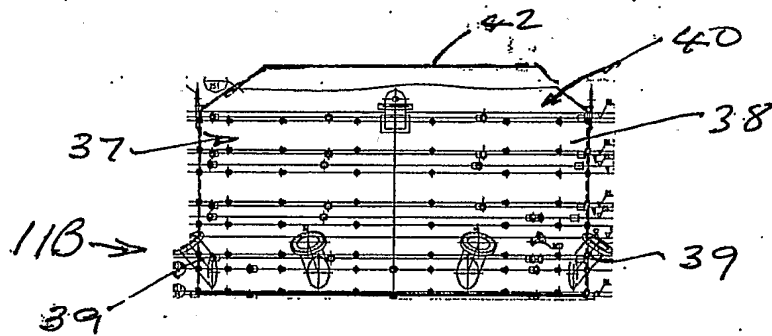


FIG. 6

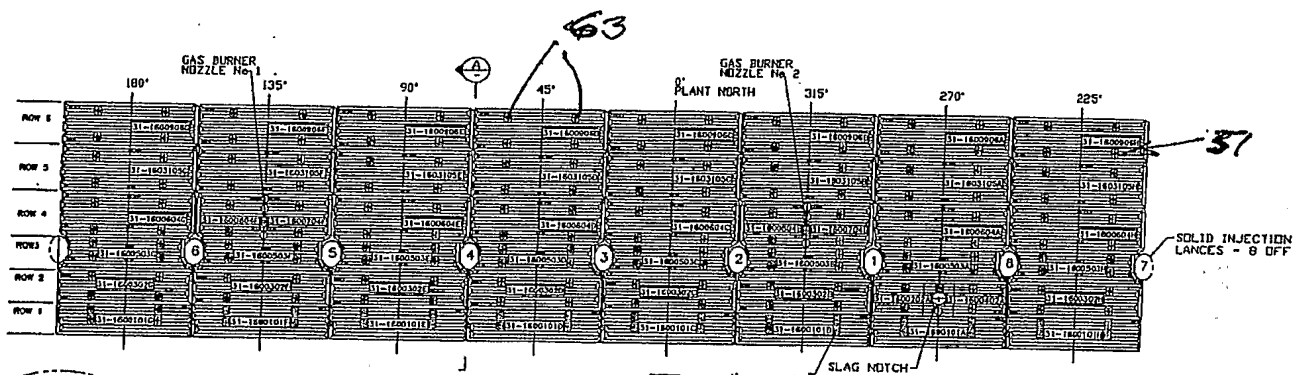


FIG. 9

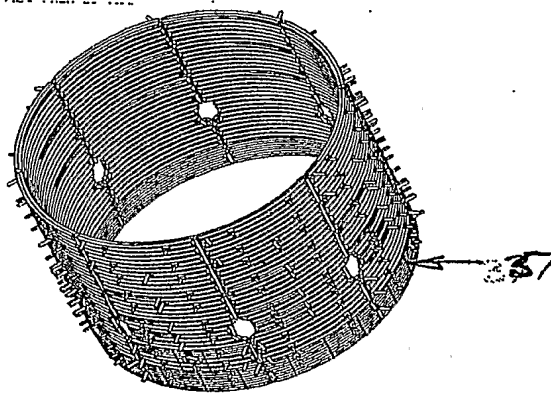


FIG. 8



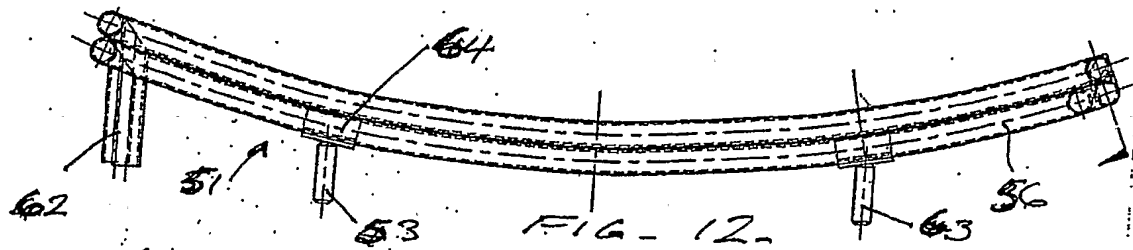


FIG. 12.

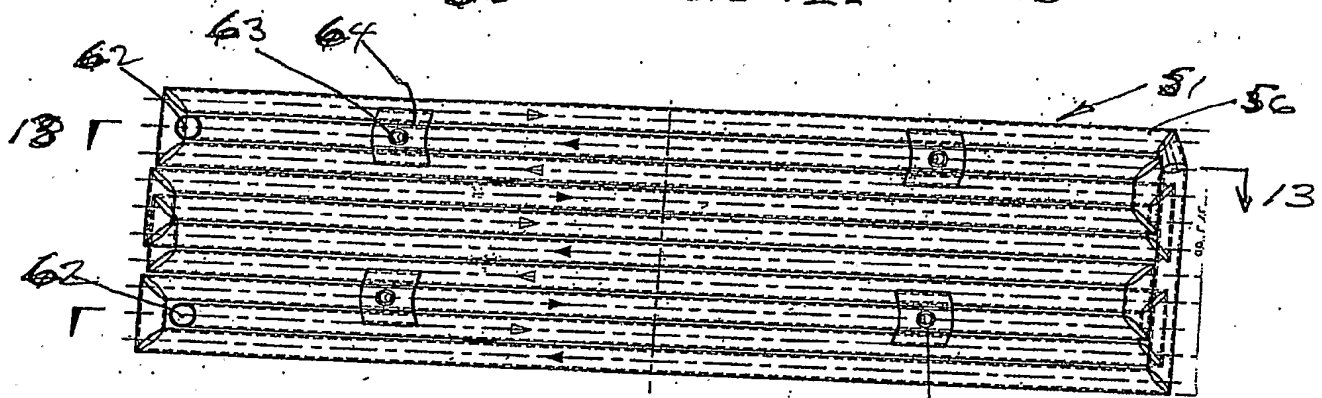


FIG. 11.



FIG. 13.

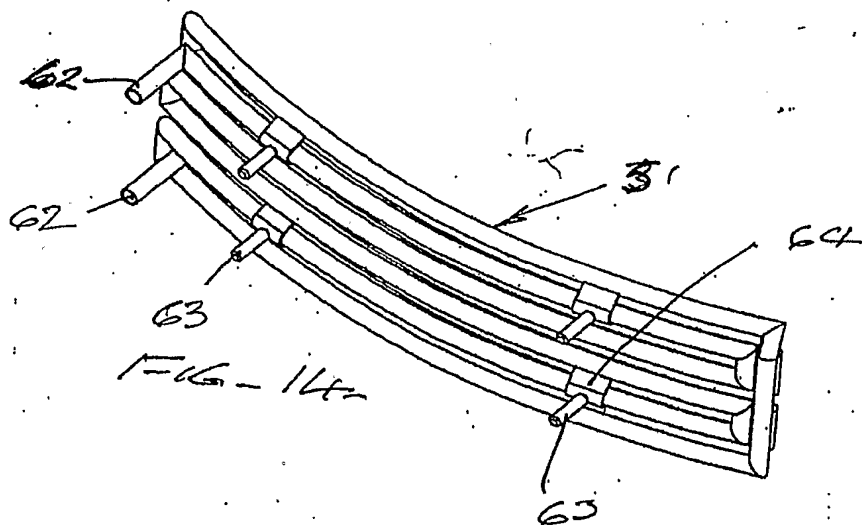


FIG. 14.

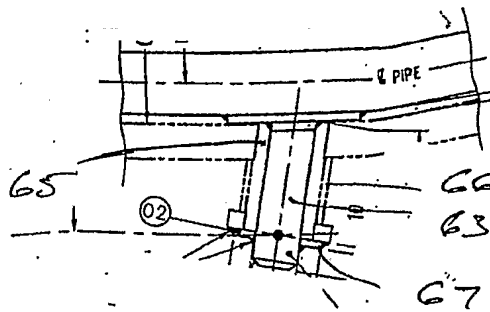


FIG- 17

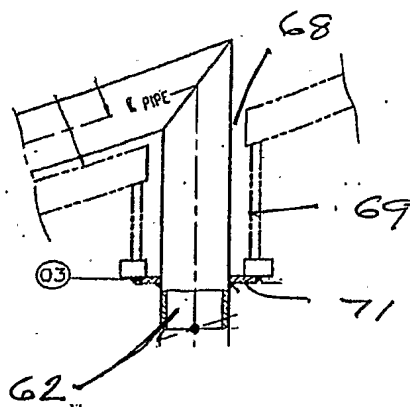


FIG. 16

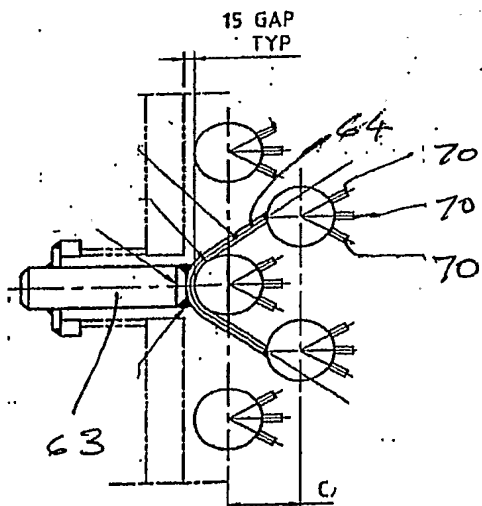


FIG. 15

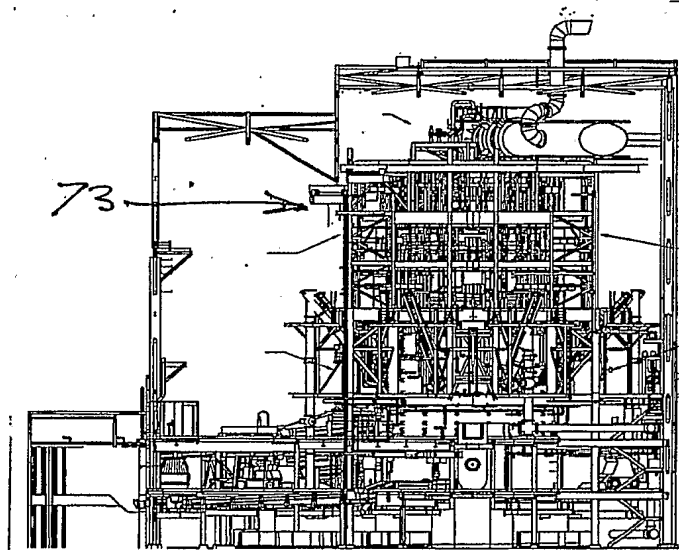


FIG. 19.

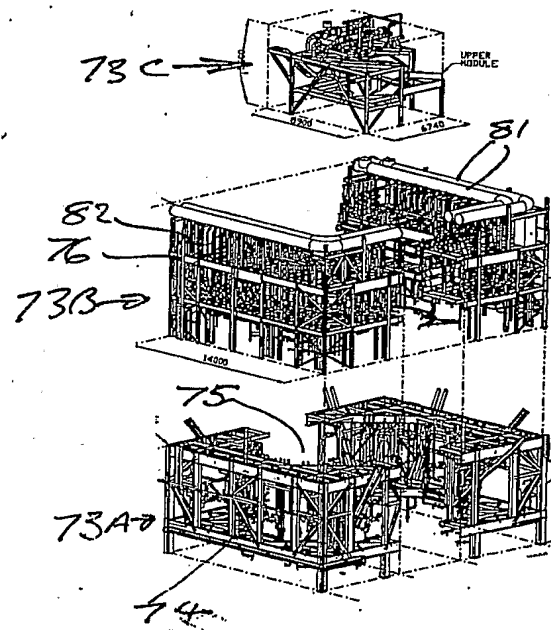


FIG. 18.